The Wilfley Table, I.

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(Toronto Meeting, July, 1907.)

This truly remarkable machine was built on a preliminary scale in May, 1895. The first full-sized table was built by Mr. A. R. Wilfley, and was used in his own mill in Kokomo Colo., in May, 1896. The first table sold for installation was placed in the Puzzle mill, Breckinridge, Summit county, Colo., in August, 1896.

The mill enthusiasts at first hailed it as the cure for all the ills that flesh is heir to in the milling line. A little later it was found to make losses which were serious, and on this account the table succeeded only to a limited extent in displacing the vanners of the gold-mills. Still later, mill-men in a number of districts throughout the country made special studies of the faults of the machine, and devised a number of ways of grouping supplementary machines to overcome as far as possible the losses, and at the same time retain the benefit of the extraordinarily large capacity accompanied by the production of clean concentrates for which the machine has become so justly famous. I hope to make an exhibit of some of these methods in an appendix to my book on ore-dressing which is now in preparation. These experimenters have not written up the subject, and if they possess all the facts they have not given them out for the benefit of the mining profession at large.

The object of this paper is to obtain the facts and to present them so clearly that their bearing can be seen by all. To this end two complete series of tests have been planned. One (the present paper), to study concentration of galena in presence of quartz; the other (to follow shortly), to study concentration of chalcopyrite in presence of quartz.

Some authorities claim that the table does its best work when treating natural products; by this phrase I mean products which have been crushed to pass through a limiting

sieve, but have had no other preparation whatever; in consequence they have all sizes of grains of both the heavy valuable mineral and the light waste gangue, ranging from the largest grains that can pass through the sieve down to the finest dust.

Others claim that the ore fed to a Wilfley table should be closely sized before it is fed. That is to say, it should be divided by a series of sieves ranging from coarse to fine into a series of products with sizes of grain ranging from coarse grains to fine grains; and that each of these products, in which the grains of the heavy mineral are of approximately the same diameter as the grains of the light mineral, should be fed to the Wilfley table.

Still a third group of authorities claims that the ore before being fed to a Wilfley table should be classified by a hydraulic classifier, which divides the crushed ore into a series of products ranging, like the sized products, from coarse grains to fine grains, by carrying it in a water-current over a series of apertures or vertical pipes, called sorting-columns, up through which water-currents are passing. These currents are graded from faster to slower, and therefore allow only the heaviest grains to settle down through the first sorting-column and out through the spigot, while lighter smaller grains settle in the second, and still lighter in the third, and so on, diminishing until the last sorting-column and spigot give very small grains, and the overflow has the finest grains of all. The classified products differ greatly from the sized products in that the grains of heavy mineral are much smaller in diameter than the light grains with which they settle, and therefore behave in a somewhat different way upon the Wilfley table from the sized products. It should be said that the first spigot-product of a classifier differs from the others in having coarse grains of heavy mineral present also.

The usual division of products upon a Wilfley table is easily and naturally made, as shown in Fig. 1, A being concentrates; B, middlings; C, tailings, and D, slimes. Of these, when natural products are fed, the concentrates, A, are nearly clean heavy mineral, a slight contamination of small grains of quartz being present. The middlings, B, carry some large grains and also some small grains of heavy mineral. The tail-

ings, C, carry some very small grains of heavy mineral, and the slimes, D, carry very minute grains of heavy mineral.

I believe that the small grains of heavy mineral in middlings, B, and tailings, C, are of less diameter than the smallest in the concentrates, A, and of greater diameter than the majority in the slimes, D, and that they belong in middlings and tailings from the law of their existence. The re-running of such middlings upon the same table is therefore not a wise proceeding, and only admissible as an expedient in small establishments when the quantity of middlings is not sufficient to warrant other provision. So much for the speculation before the investigation was made.

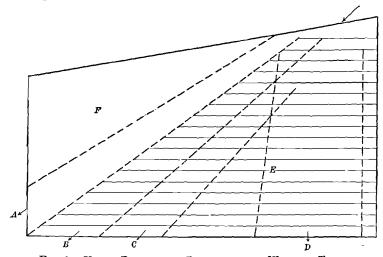


Fig. 1.—Usual Division of Products on a Wilfley Table.

The materials for this test were pure white massive quartz for the light mineral, and crystalline galena, nearly free from blende and other impurities, from Joplin, Mo., for the heavy mineral. The quantities of these impurities were so small as to have little effect on the results. Both minerals were broken down to 2-mm. size, and mixed so as to have approximately 10 per cent. of galena and 90 per cent. of quartz.

The Wilfley table used for the tests had a net working-surface of 2 ft. by 4 ft. This is the table that has been found very satisfactory for students' work at the Massachusetts Institute of Technology. An error is present to a slight extent in the full-sized table, 16 ft. long by 7 ft. wide, and to a serious ex-

tent in the small Wilfley testing-table, 7 ft. long, found in some of the schools. It is due to tacking tapered riffle-cleats on to a linoleum plane surface, thereby making two planes: first, the roughing-plane over the riffle-cleats, E, Fig. 1; second, the cleaning-plane or part where there are no riffles, F, Fig. 1. These two planes make an angle with each other, or a slight trough, which heaps up the sands deeper than is wise along the line of the tips of the riffle-cleats. This error is completely overcome on the little table here used by cutting the riffles down into the wooden surface of the table. The roughing-and cleaning-planes are therefore one and the same plane. By observing this precaution I believe that this little table is able to do as good work as the full-sized table.

Comparing the little table with the full-sized table as to areas and capacity, assuming that their capacities are proportional to their areas, we have Table I.

Table I.—Area and Capacity of Small and Large Wilfley Tables.

		Li	ttle Table.	I	arge Table.
Area,		8	sq. ft.	112	sq. ft.
Feed,		1	kg. per min.	22	tons per 24 hr.
Feed,		0.75	kg. per min.	16.6	tons per 24 hr.
Feed,		0.5	kg. per min.	11	tons per 24 hr.

These figures represent the usual range used in practice.

Seventeen runs in all were made; Nos. 1 to 5, inclusive, were made upon natural products, the several feed-products being 2 mm. to 0; 1 mm. to 0; 0.5 mm. to 0; 0.25 mm. to 0; and 2 mm. to 0. Run No. 5, although fed with the same size as No. 1, was fed at a different rate. In making these runs no effort was made to re-run the middlings; first, because the concentrates and tailings would both have been contaminated and would not have shown as well; second, because the middlings themselves would have undergone a change in composition. In consequence of this ruling, the quantities of middlings appear abnormally large.

In these runs the dividing-line between concentrates and middlings was chosen so as to make concentrates nearly clean to the eye. The dividing-line between middlings and tailings was chosen so as to keep all the large grains of heavy mineral in the middlings. The four products—concentrates, middlings,

tailings and slimes—were sized on a series of sieves, and the quartz in them determined by dissolving out the galena in hydrochloric acid. The galena was determined by difference.

Runs Nos. 6 to 11, inclusive, were all upon sized products, and the results obtained are given in Table II.

Table II.—Sizes and Weights of Materials Fed to Table.

Tests Nos. 6 to 11.

D			t -t1 Mind-ship
Run Number.	Sieves Dia Through, mm.	on, mm.	Actual Weights Fed. kg.
6	2	1.4	12.15
7	1.4	1.0	6.74
8	· 1	0.75	4.93
9	0.75	0.50	2.85
10	0.50	0.36	1.70
11	0.36	0.28	1.55
	0.28	0.00	3.08
			
			33.00

The total quantity weighed 33 kg., of which 30 kg. was quartz and 3 kg. was galena. The guiding was done simply to make clean concentrates and tailings. The middlings were in every case re-run until they could not be further reduced without contaminating the concentrates or the tailings. Where a sized ore is free from included grains and from any middle-weight mineral, the feeding-back of the middlings on the same table is logically good practice, because the middlings product is simply a mixture of concentrates and tailings; therefore, they could be fed back on the same table and disappear entirely without harm to concentrates or tailings.

Runs Nos. 12 to 17, inclusive, were made upon sorted or classified products. The classifier, Fig. 2, had 12 closed spigots or blind spigots; that is to say, spigots which discharged sand into 2-gallon bottles as fast as it came, but discharged no water. The sorting-columns were of 0.5-in. pipe, squared at the top and 3 in. long. Expressed in mm. per second, the rising-currents in the successive sorting-columns were: 105, 85, 69, 55, 45, 36, 29, 23, 19, 15, 12, 10, respectively. The 13th spigot had no rising-current, and it was simply a safety spigot to prevent any accumulation of sand that was too light to go down in the 12th and too heavy to go over into the overflow. This apparatus gives a set of products beautifully classified.

To define the classified products more completely, a small aliquot part of each was sized, photographed and analyzed. The photograph, Fig. 3, shows to the eye the distribution of sizes in each spigot. Table III. shows the distribution of quartz and galena in the different sizes of each spigot. Expressed in mm., the sieve-sizes used were: 2.83, 2.49, 2.06, 1.63, 1.44, 1.27, 1.10, 0.97, 0.84, 0.68, 0.57, 0.45, 0.36, 0.28, 0.24, 0.20, 0.15, 0.12, 0.10, 0.08. The middlings picked out and weighed for the first four spigots consisted of blende-galena included

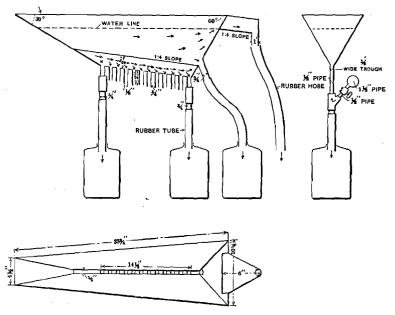


Fig. 2.—Classifier Used for Runs Nos. 12 to 17.

grains, with some free blende-grains. Their use here is simply to show how nearly pure the galena was. The settling-ratios are of special interest; for example, at the foot of spigot No. 4 we have the settling-ratio, 3.26, which signifies that in spigot No. 4 the average diameter of the quartz-grains is 3.26 times the average diameter of the galena-grains. The method of computing these ratios is given in my paper, Close Sizing Before Jigging. It was thought wiser to combine the spigots

¹ Trans., xxiv., 449, 450 (1894).

Table III.—Distribution of Quartz and Galena in Runs Nos. 12 to 17.

Run No		-	12			13	1			14	:			
No. of Spigo	ot		1			2			3	1		4		
Actual Weig	ght in kg		15.110			15.775			11,175			5.170		
Rising Cur per sec			105.		85. 69.			55.	55.					
Through mm.	On mm,	Quartz.	Galena.	Mid- dlings.										
2.83	2.49	0.052	0.004	0.007										
2.49	2.06	2.408	0.709	0.021	1.517			0.213					********	
2.06	1.63	17.170	7.216	0.085	20,299		0.006	3.617		0.003	0.112			
1.63	1.44	9.885	7.650	0.112	20.805	0.004	0.009	6.510	0.002	0.003	0.394			
1.44	1.27	9.381	8.476	0.118	19.856	0.003	0.013	12.635	0.003	0.004	1.210		 •••••••	
1.27	1.10	2.480	3.391	0.010	15.746	0.004	0.016	14.249	0.002	0.002	3.475		0.001	
1.10	0.97	1.945	3.742	0.022	5.161	0.006	0.011	14.339	0.003	0.001	2.573		0.001	
0.97	0.84	2.041	5.435	0.025	5.925	0.037	0.023	15.208	0.027	 	9.530	0.006		
0.84	0.68	0.861	3.914	0.020	2.734	0.063	0.017	10.646	0.018		12.793	0.008		
0.68	0.57	0.535	3.479	0.009	1.527	0.147	0.013	7.499	0.030		20.128	0.037		
0.57	0.45	0.356	4.143		1.558	0.865		8.795	0.167		26.312	0.056		
0.45	0.36	0.100	1.634		0.217	0.678		1.437	0.203		9.741	0.070		
0.36	0.28	0.068	1.407		0.107	1.215		0.942	0.678		6.502	0.275		
0.28	0.24	0.022	0.457		0.028	0.517		0.190	0.455	····	1.638	0.489		
0.24	0.20	0.016	0.258		0.015	0.414	{	0.124	0.825		0.667	0.892		
0.20	0.15	0.010	0.145		0.009	0.233		0.045	0.594		0.223	1.107	-	
0.15	0.12	0.007	0.089		0.005	0.107		0.013	0.295	J	0.068	0.715	· · · · · · · · · · · · · · · · · · ·	
0.12	0.10	0.001	0.018		0.003	0.025		0.007	0.093		0.037	0.458	\····	
0.10	0.08	0.007	0.037		0.005	0.029		0.010	0.102	····	0.025	0.301		
0.08	0.00	0.007	0.057		0.009	0.023	•••••	0.090	0.050	(<u></u>	0.012	0.132	····	
Total	Total		4.546	0.002										
Settling-ratio 1.58		1.58		4.11				3.93		3.26				

Run No.	•••••			.5				16	 i						17		_ 		-
No. of S	pigot	5	,	(3		7		8	[9	1	0		11		12	Ove	rflow.
Actual in kg	Weight	2.2	80	1.9	950	1.1	82	0.:	389	0.	962	0.7	165	0.0	551	0.	705	1.8	360
Rising C	urrent, er sec	45	5. 	3	6.	29	9.	2	3.	1	9.	1	5.	1	2,	1	0.		
Thro'h mm.	On mm,	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz,	Galena.	Quartz	Galena.
2.83	2.49									-							;		
$\frac{2.83}{2.49}$	2.49		•••••										• • • • • • • • •					•••••	
2.06	1.63																	• • • • • • • • • • • • • • • • • • • •	
1.63	1.44	1																	
1.44	1.27	0.031	• • • • • • • • • • • • • • • • • • • •																
1.27	1.10	0.132													 .		·		
1.10	0.97	0.184		0.015		0.008													
0.97	0.84	1.467		0.082		0.017	ļ		ļ						1		• • • • • • • • • • • • • • • • • • • •		
0.84	0.68	5.161		0.949		0.042											•••••		
0.68	0.57	5.200	0.009	1.668	ļ	0.220				0.010							•	• • • • • • • • • • • • • • • • • • • •	
0.57	0.45	29.990	0.057	16.732	0.000	3.133		0.150		0.073		0.026	• • • • • • • • •	•••••	• • • • • • • • •				
0.45	0.36	25.038	0.026		0.380	$9.086 \\ 36.110$		5.156 20.250		$1.850 \\ 13.185$			0.171	1.251	0.015	0.114	0.014	0.160	0.000
0.36	$0.28 \\ 0.24$	19.164 4.779	0.119 0.132	34.011 9.752		15.539		20.250 23.252		14.806	0.291	3.980			0.104			$0.169 \\ 0.185$	$0.238 \\ 0.195$
0.28	$0.24 \\ 0.20$	2.280	0.132	8.884		17.499		26.435		29.790		23.061		12.375				0.183	0.195
$\begin{array}{c c} 0.24 & \\ 0.20 & \end{array}$	0.20	0.725	1.019	2.171	0.406		0.296			17.320		29.820		25.773	0.223			2.243	0.438
0.15	0.12	0.720	1.612	1.011	1.273	3.344						18.685		26.653		21.415			
0.12	0.12	0.119	0.663			0.650							0.329			11.464			
0.10	0.08	0.018	0.474				2.111	0.951					1.186	7.787		20.500		28.520	1.805
0.08	0.00	0.048	0.879	0.046			1.647	0.225	1.902			1.700	4.744	3.529	5.182	17.475	4.982	35.460	
Total		$\overline{94.578}$	5.425	94.208	5.781	$\overline{93.510}$	6.486	93.815	6,157	92.837	6.261	92.887	7.102	$\overline{92.944}$	7.043	88.172	11.922	85.991	14.006
Settling	g-ratio.	3.	 19	2.	62	2.	49	2.	21	2.	21	2.	74	2.	46	1.	.28	1.	.10

somewhat instead of making 12 separate runs; accordingly, the 6 runs were fed with products as follows: 1st spigot; 2d spigot; 3d and 4th together; 5th and 6th together; 7th, 8th and 9th together; 10th, 11th and 12th together.

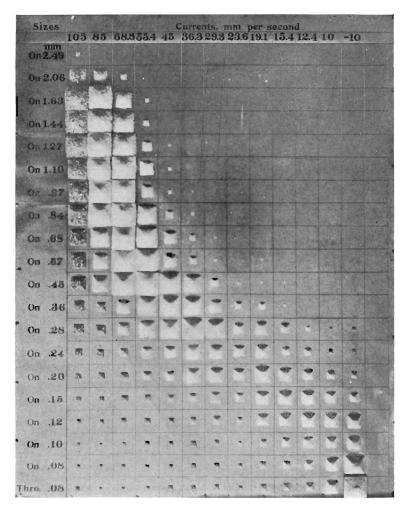


Fig. 3.—Distribution of Sizes by the Classifier.

The first 5 runs on natural products computed on the basis of a 100-ton lot, and to the rate of feeding of a full-sized table, gave products shown in Table IV.

				Run No. 1.	Run No. 2.	Run No. 3.	Run No. 4.	Run No. 5.
Size	of F	eed.		mm. 2 to 0.	mm. 1 to 0.	mm. 0.5 to 0.	mm. 0.25 to 0.	mm. 2 to 0.
Rate of fee	d pe	er 24	hours,	Tons. 22.	Tons. 22.	Tons.	Tons. 11.	Tons.
Concentrate	es,			4.114	2.973	4.667	5.343	2.808
Middlings,				21.486	20.750	25.981	21.028	45.538
Tailings,				72.856	72.903	62.813	60.487	50.688
Slimes,				1.544	3.374	6.539	13.142	0.966
Total,				100.000	100.000	100.000	100.000	100.000

The next 6 runs on sized products, computed on the basis of a 100-ton lot, and to the rate of feeding of a full-sized table, gave products shown in Table V.

TABLE V.—Results of Runs Nos. 6 to 11.

		Run No. 6.	Run No. 7.	Run No. 8.	Run No. 9.	Run No. 10.	Run No. 11.
Size of Feed	l , .	$\begin{array}{c} \text{mm.} \\ 2.00 \\ \text{to 1.4} \end{array}$	mm, 1.4 to 1.0	mm. 1.0 to 0.75	mm. 0.75 to 0.50	mm, 0.50 to 0.36	mm. 0.36 to 0.28
	_	Tons.	Tons.	Tons.	Tons.	Tons.	Tons.
Rate of feed p	er 24						
hours,.		22.	16.6	11.	11.	11.	11.
Concentrates, .		6.537	9.728	12.064	13.168	12.171	15.137
Middlings,		1.647	1.901	1.694	1.602	5.310	3.170
Tailings,		91.816	88.371	86.242	85.230	82.519	81.693
Slimes,		0.000	0.000	0.000	0.000	0.000	0.000
Total, .		100.000	100.000	100.000	100.000	100.000	100.000

The last 6 runs, computed on the basis of 100-ton lots, and to the rate of feeding of a full-sized table, gave products shown in Table VI.

Table VI.—Results of Runs Nos. 12 to 17 Computed to Full-Sized Table

		~~~~~	ace.			
	Run No. 12.	Run No. 13.	Run No. 14.	Run No. 15.	Run No. 16.	Run No. 17.
Classifier spigots, numbers that were fed, . Classifier currents, mm. per second through	1.	2.	3, 4.	5, 6.	7, 8, 9.	10, 11, 12.
which grains settled,	105.	85.	55.4	36.3	19.1	10.
Rate of feed to Wil-	Tons.	Tons.	Tons.	Tons.	Tons.	Tons.
fley, 24 hours, .	11.	11.	16.6	11.	11.	11.
Concentrates,	49.649	3.950	3.398	4.940	5.7165	4.980
Middlings,	5.534	1.307	0.663	0.828	1.0435	4.262
Tailings,	44.817	94.743	95.939	94.232	93.240	90.758
Slimes,	0.000	0.000	0.000	0.000	0.000	0.000
Total,	100.000	100.000	100.000	100.000	100.000	100.000
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Comparing the 17 runs as to quantity of the products without looking at the quality, it will be noticed at once that the concentrates and tailings in runs Nos. 6 to 11 and Nos. 12 to 17 are very much larger in quantity than these products in runs Nos. 1 to 5; while the middlings are very much smaller in quantity.

A comprehensive table of all 17 runs is given in Table VII., which shows the proportions of concentrates, middlings, tailings and slimes in each, and also the percentage of galena and quartz in the various products.

Tables VIII., IX., X. and XI. give the weights in tons of the different sizes, and also the proportion of quartz and galena in each product by sizes.

In comparing the analyses of the concentrates of these five runs (Table VIII.), we see a very remarkable similarity in the behavior of the quartz and galena through all five runs. The coarser sizes and the finer sizes are almost clean galena, being nearly free from quartz. At a point somewhere a little below the middle, the quartz rises to a maximum, which in the first run reaches 18.99 per cent. of quartz, in the third run reaches 7.38 per cent. of quartz, and in the fifth run reaches 13.80 per cent. of quartz.

Comparing the different analyses of the middlings (Table IX.), we find the galena among the very largest and smallest grains gives a very high percentage, and down to a little below the middle the galena runs down to a very low percentage, while the quartz behaves just in the opposite way. This is analogous to the composition of the concentrates.

Comparing the tailings of the five runs (Table X.), we note that the galena appears only to a very slight degree in any of the tailings until we get down to the smaller sizes, and there we have figures that rise to an almost alarming size, the first run giving 17.5 per cent. of galena in the finest size; the 2d, 17.8 per cent.; the 5th run giving 12.17 per cent. in the finest size.

The slimes (Table XI.), which have a serious quantity of material only in the finest size, have also a serious percentage of lead in that finest size. The other percentages of lead are generally much smaller. There are three exceptions, in the 2d, 3d and 4th runs, where the percentages run high in the larger

Table VII.—Summary of Results of Runs Nos. 1 to 17.

		Rate		Compos	ition of	Perce	ntage of	the Pro	ducts.			Com	position	of Prod	ucts.			Per	Cent. of	Total Ga	lena.	Quantity ally Fed.
of Run	Size.	Kg. Per Min.	24 hrs. Table.	the	Feed.	Concen- trates.	Mid-	Tail-	Slimes,	Conce	ntrates.	Midd	lings.	Tail	ings.	Slir	nes,	Concen- trates.	Mid-	Tail-	Slimes,	l Qua
No.		X. M.	Tons la'ge	Quartz.	Galena.	Con	dlings.	ings.	),,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena,	l oo st	dlings.	ings.	onnes.	Total Actue
1	2 to 0	1	22	Per Ct. 90.91	Per Ct. 9.09	Per Ct. 4,11	Per Ct. 21.48	Per Ct. 72.87	Per Ct. 1.54	Per Ct. 9.92	Per Ct. 90.08	Per Ct. 76.42	Per Ct. 23.58	Per Ct. 99.49		Per Ct. 81.10	Per Ct. 18,90	Per Ct. 39.20	Per Ct. 53, 34	Per Ct. 3.82	Per Ct. 3.64	Kg.
2	1 to 0	1	22	90.91	9.09	2.97	20.75	72.91	3.37	8.50	91.50	73.37	26.63	99.39		90.29	9.71	34.58	57.34	4.72		11
3	0.5 to 0	0.5	11	90.91	9.09	4.67	25.98	62.81	6.54	2.40	97.60	84.10	15.90	99.10	0.90	87.82	12.18	44.86	41.98	5.44	7.72	11
4	0.25 to 0	0.5	11	90.91	9.09	5.34	21.03	60.49	13.14	2.27	97.73	87.16	12.84	98.39	1.61	90.04	9.96	51.48	27.59	8.20	12.73	11
5	2 to 0	0.5	11	90.91	9.09	2.80	45.67	50.30	1.23	4.66	95.34	86.29	13.71	99.71	0.29	85.38	14.62	29.06	67.79	1.62	1.53	9.63
6	2 to 1.4	1	22	92.60	7.40	6.54	1.65	91.81		0.77	99.23	40.33	59.67	99.96	0.04			87.43	12.05	0.52		12.08
7	1.4 to 1	0.75	16,6	89.08	10.92	9.73	1.90	88.37		0.77	99.23	76.90	23.10	100.00				96.43	3.57	0.00		6.74
8	1 to 0.75	0.5	11	87.32	12.68	12.06	1.69	86.25		0.99	99.01	83.00	17.00	99.91	0.09		• • • • • • • •	97.62	1.80	0.58		4.93
9	0.75 to 0.5	0.5	11	87.15	12.85	13.15	1.60	85.25		2.50	97.50	77.40	22.60	99.65	0.35			96.58	2.29	1.13		2.845
10	0.5 to 0.36	0.5	11	85.92	14.08	12.18	5.31	82.51		0.69	99.31	80.03	19.97	99.76	0.24			90.57	7.95	1.48		1.72
11	[0.36 to 0.28]	0.5	11	85.70	14.30	15.10	3.17	81.73		2.14	97.86	84.67	15.35	99.56	0.44		• • • • • • • • • • • • • • • • • • • •	94.60	3.10	2.30	· · · · · · · · · · ·	1.59
	Classifier.	. 1	1									[										
12	1st spigot		11	49.82	50.18	49.65	5.53	44.82		0.74	99.26	86.15	13.85	99.71	0.29	• • • • • • •	• • • • • • • • • • • • • • • • • • • •	98.21	1.53	0.26		13.60
13	2d "	0.5	11	95.21	4.79	3.95	1.31	94.74	. <b></b>	1.38	98.62	66.05	33.95	99.64	0.36			81.35	10.72	7.93		14.197
14			16.6	96.23	3.77	3.40	0.66	95.94		1.15	98.85	65.57	34.43	99.80	0.20	• • • • • • • • • • • • • • • • • • • •		88.95	5.98	5.07	•••••	14.629
	5 and 6 "	0.5	11	94.39	5.61	4.94	0.83	94.23		1.65	98.35	71.10	28.90	99.45	0.55	•••••	• • • • • • • •	86.66	4.29	9.05		3.745
16	7, 8, 9 "	0.5	11	93.74	6.26	5.72	1.04	93.24	•••••	1.16	98.84	83.75	16.25	99.54	0.46	•••••	• • • • • • • • • • • • • • • • • • • •	90.58	2.90	6.52		2.28
17	10,11,12 ''	0.5	11	93.73	6.27	4.98	4.26	90.76	<u></u>	0.38	99.62	83.72	16.28	99.34	0.66	• • • • • • • • • • • • • • • • • • • •		79.38	10.69	9.93		1.9

Table VIII.—Proportion of Quartz and Galena in Products.

Note.—Concentrates sized and weighed. The weights are computed in tons and fractions of a ton on the 100-ton basis.

Sizes	3.	7		_		70
Through.	On.	Run No. 1.	Run No. 2.	Run No. 3.	Run No. 4.	Run No. 5.
mm.	mm. 2.06	Tons. 0.017	Tons.	Tons.	Tons.	Tons. 0.009
2.06	1.63	0.059				0.037
1.63	1.44	0.066				0.054
1.44	1.27	0.112			·	0.076
1.27	1.10	0.084				0.049
1.10	0.97	0.120	0.003			0.079
0.97	0.84	0.174	0.012			0.104
0.84	0.68	0.206	0.027			0.128
0.68	0.57	0.245	0.048			0.138
0.57	0.45	0.506	0.280	0.225		0.288
0.45	0.36	0.402	0.141	0.322		0.201
0.36	0.28	0.445	0.465	1.000	0.227	0.303
0.28	0.24	0.306	0.304	0.386	0.081	0.179
0.24	0.20	0.375	0.370	0.586	0.760	0.230
0.20	0.15	0.307	0.324	0.483	0.997	0.218
0.15	0.12	0.209	0.313	0.483	0.958	0.213
0.12	0.10	0.110	0.207	0.271	0.397	0.082
0.10	0.08	0.189	0.235	0.404	0.871	0.229
0.08	0.00	0.182	0.244	0.507	1.052	0.191
otal tons		4.114	2.973	4.667	5.343	2.808

Analyses of the above products giving percentages of galena (PbS) and quartz (SiO₂).

Si	es.	Run	No. 1.	Run	No. 2.	Run	No. 3.	Run	No. 4.	Run	No. 5.
Thro.	On.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.
mm.	mm.	Per Ct.	Per Ct.	Per Ct.	Per Ct.	Per Ct.	Per Ct.				
• • • • • • • • • • • • • • • • • • • •	2.06	100.00	0.00							100.00	0.00
2.06	1.63	99.77	0.23		•••••					97.56	2,44
1.63	1.44	99.80	0.20							100.00	0.00
1.44	1.27	99.88	0.12							99.87	0.13
1.27	1.10	99.76	0.24			1		! . • • • • • • • • • •		99.29	0.71
1.10	0.97	99.43	0.57	100.00	0.00	<b>.</b>	·			99.28	0.72
0.97	0.84	98.42	1.58	99.72	0.28				. <b></b>	99.80	0.20
0.84	0.68	96.54	3.46	99.90	0.10			·		99.5 <b>5</b>	0.45
0.68	0.57	94.47	5.53	100.00	0.00					99.52	0.48
0.57	0.45	91.05	8.95	100.00	0.00	99.61	0.39			97.67	2,33
0.45	0.36	83.81	16.19	99.81	0.19	99.71	0.29		l	93.34	6.66
0.36	0.28	81.24	18.76	99.74	0.26	99.48	0.52	96.56	3.44	89.24	10.76
0.28	0.24	81.01	18.99	99.16	0.84	99.36	0.64	96.67	3.33	86.20	13.80
0.24	0.20	84.39	15.61	98.25	1.75	97.81	2.19	99.24	0.76	88.21	11.79
0.20	0.15	89.48	10,52	98.02	1.98	93.14	6.86	98.54	1.46	92.92	7.08
0.15	0.12	95.08	4.92	98.78	1.22	92.62	7.38	96.84	3.16	97.52	2.48
0.12	0.10	95.08	4.92	99.32	0.68	95.35	4.65	95.54	4.46	99.03	0.97
0.10	0.08	97.74	2.26	99.57	0.43	98.71	1.29	96.66	3.34	99.65	0.35
0.08	0.00	99.45	0.55	99.62	0.38	99.40	0.60	98.72	1.28	99.63	
Total centi	con- }	90.08	9.92	91.50	8.50	97.60	2.40	97.73	2.27	95.34	4.66

Table IX.—Proportion of Quartz and Galena in Products.

NOTE.—Middlings sized and weighed and the weights computed in tons and fractions of a ton on the 100-ton basis.

		<u> </u>	<u> </u>	\	
Size.	Run	Run	Run	Run	Run
On.	No. 1.	No. 2.	No. 3.	No. 4.	No. 5.
mm.	Tons,	Tons.	Tons.	Tons.	Tons.
2.06	0.132			.,	0.206
1.63	0.795				1.595
1.44	0.783				2.134
1.27	1.202		 		2.986
1.10	0.954				2.438
0.97	1.056	0.292			3.178
0.84	1.552	1.330			4.793
0.68	2.021	0.329			5.113
0.57	1.865	1.350			4.323
0.45	3.112	3.203	2.171		8.871
0.36	2.326	2.680	3.117		3.144
0.28	2.526	3.945	5,955	0.402	3.655
0.24	0.848	1.436	4.805	1.684	1.079
0.20	1.230	2.932	3.698	4.729	0.969
0.15	0.648	1.551	4.362	4.713	0.581
0.12	0.207	0.893	0.481	3.660	0.223
0.10	0.075	0.299	0.418	2.296	0.050
0.08	0.061	0.286	0.601	2.216	0.054
0.00	0.093	0.224	0.373	1.328	0.146
Total tons	21.486	20.750	25.981	21.028	45.538

Analyses of the above products giving percentages of galena (PbS) and quartz (SiO₂).

Size.	Run	No. 1.	Run	No. 2.	Run	No. 3.	Run	No. 4.	Run	No. 5.
On.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.
mm.	Per Ct.	Per Ct.		1	1		Per Ct.		Per Ct.	Per Ct.
2.06	73.47	26.53							38.43	61.57
1.63	75.39	24.61							41.68	58.32
1.44	69.47	30.53	1							69.79
1.27	62.80	37.20								77.31
1.10	54.75	45.25								81.96
0.97	43.80	56.20	90.46							86.15
0.84	31.40	68.60	89.46	10.54					11.43	88.57
0.68	20.10	79.90	81.60	18.40			¦	• • • • • • • • • • • • • • • • • • • •	9.92	90.08
0.57	16.70	83.30	69.23	30.77	ļ				9.60	90.40
0.45	11.30	88.70	37.50	62.50	66.66	33.34		:  ••••••	9.07	90.93
0.36	8.11	91.89	20.22	79.78	23.67	76.33			8.40	91.60
0.28	6.44	93.56	12.81	87,19	14.10	85.90	29.43	70.57	8.36	91.64
0.24	4.92	95.08	8.41	91.59	6.60	93.40	19.74	80.26	7,75	92.25
0.20	3.68	96.32	7.26	92.74	5.16	94.84	11.78	88.22	8.27	91.73
0.15	4.44	95.56	5.36	94.64	5.01	94.99	8.25	91.75	10.20	89.80
0.12	6.65	93.35	4.49	95.51	6.56	93.44	7.10	92.90	17.39	82.61
0.10	7.26	92.74	7.45	92.55	6.46	93.54	6.81	93.19	26.88	73.12
0.08	32.23	67.77	11.72	88.28	10.24	89.76	9.22	90.78	58.90	41.10
0.00	90.46	9.54	48.33	51.67	70.76	29.24	51.84	48.16	90.87	9.13
Total midd.	23.58	76.42	26.63	73.37	15.90	84.10	12.84	87.16	13.71	86.29

Table X.—Proportion of Quartz and Galena in Products.

Note.—Tailings sized and weighed and the weights computed in tons and fractions of a ton on the 100-ton basis.

Size. On.	Run No. 1.	Run No. 2.	Run No. 3.	Run No. 4.	Run No. 5.
mm.	Tons	Tous.	Tons.	Tons.	Tons.
2.06	3.777	••••••			2.003
1.63	<b>14.71</b> 3				11.883
1.44	11.145				9.065
1.27	8.085			[	10.600
1.10	6.174				4.294
0.97	7.322	11.860			4.452
0.84	5.191	16.217			1.489
0.68	3.350	8.821			0.682
0.57	2.078	5.789			0.405
0.45	2.501	11.639	20.635		0.396
0.36	1.581	4.167	11,120		0.162
0.28	1.056	3.315	10.790	0.400	0.456
0.24	0.523	0.915	2.829	2.019	0.303
0.20	0.633	2.341	3.277	12.345	0.680
0.15	0.739	1.860	3.574	11.948	1.075
0.12	1.139	1.781	4.308	9.015	0.507
0.10	0.624	1.067	1.113	6.118	0.614
0.08	0.948	1.461	2.965	9.778	0.878
0.00	1.277	1.670	2.202	8.864	0.742
Total tons	72.856	72.903	62.813	60.487	50.686

Analyses of the above products giving percentages of galena (PbS) and quartz (SiO $_2$ ).

Size.	Run	No. 1.	Run	No. 2.	Run	No. 3.	Run	No. 4.	Run	No. 5.
On.	Galena.	Quartz.								
mm.	Per Ct.		Per Ct.							
2.06	0.40	99.60							0.00	100.00
1.63	0.40	99.60							0.00	100.00
1.44	0.50	99.50	ļ						0.00	100.00
1.27	0.20	99.80						¦	0.05	99.95
1.10	0.01	99.99							0.02	99.98
0.97	0.02	99.98	0.02	99.98					0.02	99.98
0.84	0.00	100.00	0.01	99.99				·	0.03	99.97
0.68		100.00	0.00	100.00					0.01	99.99
0.57	0.00	100.00	0.00	100.00					0.08	99.92
0.45	0.00	100.00	0.00	100.00	0.00	100.00			0.05	99.95
0.36	0.08	99.92	0.12	99.88	0.16	99.84			0.68	99.32
0.28	0.12	99.88	0.16	99.84	0.64	99.36	2.95	97.05	0.80	99.20
0.24	0.69	99.31	0.26	99.74	2.03	97.97	0.41	99.59	0.74	99.26
0.20	1.24	98.76	0.80	99.20	1.19	98.81	0.69	99.31	0.82	99.18
0.15	1.45	98.55	1.40	98.60	1.49	98.51	1.00	99.00	0.76	99.24
0.12	1.82	98.18	1.89	98.11	1.65	98.35	1.26	98,74	1.16	98.84
0.10	2.88	97.12	1.69	98.31	1.60	98.40	1.76	98.24	1.71	98.29
0.08	3.43	96.57	2.60	97.40	1.51	98.49	1.49	98.51	3.00	97.00
0.00	17.50	82.50	17.85	82.15	8,55	91.45	4.28	95.72	12.17	87.83
Total tailin's	0.51	99,49	0.61	99.39	0.90	99.10	1.61	98.39	0.29	99.71

sizes, but the quantity is so small that these losses are insignificant.

Table XI.—Proportion of Quartz and Galena in Products.

Note.—Slimes sized and weighed. The weights are computed in tons and parts of a ton, on the 100-ton basis.

Size	es.	Run	Run	Run	Run	Run	
Through.	On.	No. 1.	No. 2.	No. 3.	No. 4.	No. 5.	
mm. 0.45	mm, 0.36	Tons. 0.156	Tons.	Tons.	Tons.	Tons.	
0.36	0.28	0.047			0.214	0.003	
0.28	0.24	0.036			0.026	0.004	
0.24	0.20	0.053	0.032		0.044	0.007	
0.20	0.15	0.063	0.072	0.207	0.091	0.027	
0.15	0.12	0.052	0.062	0.078	0.138	0.037	
0.12	0.10	0.068	0.149	0,241	1.515	0.038	
0.10	0.08	0.134	0.446	1.662	1.268	0.244	
0.08	0.00	0.935	2.613	4.351	9.846	0.606	
Total tons		1.544	3.374	6.539	13.142	0.966	

Analyses of the above products giving percentages of galena (PbS) and quartz (SiO2).

Size	Sizes.		Run No. 1.		Run No. 2.		No. 3.	Run	No. 4.	Run No. 5.	
Thro.	On.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.
mm.	mm.		Per Ct.	Per Ct.	Per Ct.	Per Ct.	Per Ct.	Per Ct.	Per Ct.	Per Ct.	Per Ct.
0.45	0.36	0.00	100.00								
0.36	0.28	10.20	89.80					48.54	51.46	18.30	81.70
0.28	0.24	10.00	90.00					54.55	45.45	15.40	84.60
0.24	0.20	10.81	89.19	14.04	85.96			40.22	59.78	11.80	88,20
0.20	0.15	12.58	87.42	7.94	92.06	45.21	54.79	37.16	62.84	8.10	91.90
0.15	0.12	19.00	81.00	7.26	92.74	21.21	78.79	28.96	71.04	6.50	93.50
0.12	0.10	24.28	75.72	7.19	92.81	17.53	82.47	9.37	90.63	5.00	95.00
0.10	0.08	27.04	72.96	5.03	94.97	8.53	91.47	6.87	93, 13	6.40	93,60
0.08	0.00	28.31	71.69	10.72	89.28	11.53	88.47	8.76	91.24	19.40	80.60
Total s	limes	18.90	81.10	9.71	90.29	12.18	87.82	9.96	90.04	$\overline{14.62}$	85.38

Commenting upon runs Nos. 6 to 11 (Table XII.), as compared with runs Nos. 1 to 5, we note immediately that the concentrates all the way through are almost pure galena with scarcely any quartz, and the tailings are almost pure quartz and scarcely any galena. The middlings, as remarked before, are so small in quantity that they affect the runs but little, and when we consider that they can go directly back on to the table in the continuous run, they do not affect the result at all. This set of runs, Nos. 6 to 11, therefore appears to distance runs Nos. 1 to 5 in the competition. There is really no comparison, since runs Nos. 1 to 5 are not in the same class with them.

Table XII.—Results of Runs Nos. 6 to 11 Computed to Full Size.

Note.—The weights of products have been computed in tons and fractions thereof.

	Run No. 6.	Run No. 7.	Run No. 8.	Run No. 9.	Run No. 10.	Run No. 11.
Concentrates	Tons. 6.537	Tons. 9.728	Tons. 12.064	Tons. 13,168	Tons. 12.171	Tons. 15, 137
Middlings	1.647	1.901	1.694	1.602	5.310	3.170
Tailings	$91.816 \\ 0.000$	88.371 0.000	86.242 0.000	85.230 0.000	82.519 0.000	81.693 0.000
Total	100.000	100.000	100.000	100.000	100.000	100.000

Analyses of the above products giving percentages of galena (PbS) and quartz (SiO₂).

	Run No. 6. Run No. 7.		Run No. 8. Run		5. 9. 1	Kun No. 1	0. Run No. 11.
Reconstruction   Reco	t. Cent. 99.23 23.10	Per Per Cent. Cent. 0.77 99.01 76.90 17.00 00.00 0.09	0.99 83.00	Cent. C 97.50 2 22.60 77	ent. (2.50 9 7.40 1	Per Cent. Cen 9.31 0.6 (9.24 99.1	Per Per Cent. 9 97.86 2.14 15.35 84.65

Comparing the concentrates of runs Nos. 12 to 17 (Table XIII.), we see in the first place an enormous heaping-up of concentrates in run No. 12. The weight, 49 tons, is more than double the weight of all the other five runs in this set put together. This heaping-up of the great quantity of concentrates on the table which treats the first spigot of a classifier is one of the prominent features of the use of a classifier in preparation for feeding Wilfley tables. If we look at the total percentage of galena and quartz in the concentrates of run No. 12 we see that they contain 99.26 per cent. of galena and 0.74 per cent. of quartz. This makes an extremely good showing, and one which bids for favorable consideration of the classifier set.

Looking at the later spigots, that is to say, runs Nos. 13 to 17, inclusive, in the analyses, we see that the percentage of quartz looks high in the coarser sizes. This would seem a serious disadvantage if it were not for the fact that these products which have the high percentages of quartz are so small in quantity that the quartz cuts scarcely any figure in the final percentage of quartz in the concentrates. Altogether this set

TABLE XIII .- Results of Runs Nos. 12 to 17 Computed to Full Size.

Note.—The concentrates have been sized and weighed and the weights computed in tons and fractions thereof on the 100-ton basis.

Sizes	S.	Run	Run	Run	Run	Run	Run	
Through.	On.	No. 12.	No. 13.	No. 14.	No. 15.	No. 16.	No. 17.	
mm.	mm. 2.06	Tons. 0.128	Tons.	Tons.	Tons.	Tons.	Tons.	
2.06	1.63	4.869	0.001	0.0003		·		
1.63	1.44	6.331	0.001	0.0003				
1.44	1.27	7.861	0.002	0.0003				
1.27	1.10	4.455	0.002	0.0002	0.0005			
1.10	0.96	4.093	0.002	0.0003	0.0003			
0.96	0.84	5.837	0.011	0.001	0.0003	0.0005	 	
0.84	0.68	3.674	0.036	0.002	0.0005	0.0005	0.0004	
0.68	0.57	3.615	0.124	0.006	0.001	0.001	0.0004	
0.57	0.45	4.347	0.730	0.054	0.005	0.004	0.0023	
0.45	0.36	2.063	1.208	0.174	0.012	0.007	0.004	
0.36	0.28	1.232	0.687	0.656	0.060	0.049	0.015	
0.28	0.24	0.445	0.384	0.415	0.110	0.077	0.015	
0.24	0.20	0.330	0.393	0.697	0.332	0.138	0.057	
0.20	0.15	0.152	0.223	0.701	1.176	0.220	0.108	
0.15	0.12	0.088	0.084	0.393	1.321	0.634	0.086	
0.12	0.10	0.029	0.021	0.143	0.551	0.748	0.109	
0.10	0.08	0.055	0.029	0.104	1.057	2.300	0.934	
0.08	0.00	0.045	0.012	0.052	0.315	1.539	3.650	
otal tons	tal tons		3.950	3.398	4.940	5.717	4.980	

Analyses of the above products giving percentages of galena (PbS) and quartz (SiO2).

Size.	Run	No. 12.	Run	No. 13.	Run	No. 14.	Run	No. 15.	Run No. 16.		Run No. 17.	
On.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.
mm.	Per Ct.		Per Ct.	Pèr Ct.	Per Ct.	Per Ct.	Per Ct.					
2.06	100.00	0.00						! , • • • • • • • • • •				
1.63	99.96	0.04	100.00	0.00	60.00	40.00			 			
1.44	99.96	0.04	100.00	0.00	75.00	25.00				i		
1.27	99.95	0 05	93.10	6.90	75.00	25.00				   <b></b>		
1.10	99,84	0.16	91.45	8.55	85.71	14.29	0.00	100.00				
0.96	99.69	0.31	89.69	10.31	80.00	20.00	87.50	12.50				
0.84	99.45	0.55	95.63	4.37	98.13	1.87	85.72	14.28	0.00	100.00		
0.68	99.03	0.97	96.15	3.85	97.58	2.42	50.00	50.00	63,63	36.37	50.00	50.00
0.57	98.76	1.24	97.49	2.51	97.75	2.25	50.00	50.00	88.24	11.76	33.33	66.67
0.45	97.80	2,20	98.01	1.99	96.06	3.94	73.36	26.64	88.78	11.22	93.80	6.20
0.36	97.05	2.95	98.80	1.20	96.58	3.42	20.50	79.50	92.53	7.47	96.52	3.48
0.28	96.96	3.04	98.24	1.76	98.02	1.98	95.84	4.16	93.54	6.46	98.20	1.80
0.24	96.85	3.15	98.96	1.04	98.57	1.43	97.46	2.54	97,44	2.56	98.58	1.42
0.20	97.51	2.49	99.35	0.65	99.05	0.95	98.93	1.07	96.37	3.63	99.36	0.64
0.15	97.51	2.49	99.58	0.42	99.42	0.58	99.46	0.54	96.41	3.59	99.19	0.81
0.12	98.88	1.12	99.81	0.19	99.80	0.20	99.76	0.24	97.14	2.86	97.56	2.44
0.10	97.77	2.23	99.82	0.18	99.88	0.12	99.83	0.17	98.37	1.63	96.92	3.08
0.08	97.71	2.29	99.83	0.17	99.86	0.14	99.86	0.14	99.31	0.69	99.30	0.70
0.00	96.86	3.14	99.64	0.36	99.88	0.12	99.84	0.16	99.84	0.16	99.86	0.14
Total concent's.	99.26	0.74	98.62	1.38	98.85	1.15	98.35	1.65	98.84	1.16	99.62	0.38

Table XIV.—Results of Runs Nos. 12 to 17 Computed to Full Size.

NOTE.—The middlings have been sized and weighed and the weights computed in tons and fractions thereof on the 100-ton basis.

Sizes		Run	Run	Run	Run	Run	Run	
Through.	On.	No. 12.	No. 13.	No. 14.	No. 15.	No. 16.	No. 17.	
mm.	mm. 2.49	Tons. 0.005	Tons.	Tons.	Tons.	Tons.	Tons.	
2.49	2.06	0.061	0.001					
2.06	1.63	0.788	0.015	0.002			: : ••••••••••••	
1.63	1.44	0.602	0.026	0.001				
1.44	1.27	0.951	0.037	0.002				
1.27	1.10	0.676	0.014	0.002				
1.10	0.96	0.605	0.018	0.002	0.0003			
0.96	0.84	0.758	0.078	0.005	0.0003	0.001		
0.84	0.68	0. 73	0.120	0.011	0.002	0.001	0.001	
0.68	0.57	0.263	0.194	0.033	0.003	0.003	0.001	
0.57	0.45	0.234	0.494	0.092	0.020	0.011	0.003	
0.45	0.36	0.042	0.188	0.133	0.031	0.025	0.004	
0.36	0.28	0.030	0.089	0.236	0.139	0.064	0.075	
0.28	0.24	0.015	0.014	0.048	0.093	0.070	0.080	
0.24	0.20	0.011	0.011	0.068	0.250	0.213	0.281	
0.20	0.15	0.004	0.003	0.020	0.146	0.299	0.809	
0.15	0.12	0.004	0.002	0.005	0.076	0.188	1.013	
0.12	0.10	0.001	0.001	0.001	0.015	0.051	0.53	
0.10	0.08	0.004	0.001	0.001	0.028	0.060	0.909	
0.08	0.00	0.007	0.001	0.001	0.025	0.057	0.555	
Total tons		5.534	1.307	0.663	0.828	1,043	4.262	

Analyses of the above products giving percentages of galena (PbS) and quartz ( $\mathrm{SiO}_2$ ).

Size.	Run	No. 12.	Run	No. 13.	Run	Run No. 14.		Run No. 15.		Run No. 16.		No. 17.
On.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.	Galena.	Quartz.
mm. 2.49	Per Ct. 0.00	Per Ct. 100.00	Per Ct.	Per Ct.	Per Ct.	Per Ct.	Per Ct.	Per Ct.	Per Ct.	Per Ct.	Per Ct.	Per Ct.
2.06	22.34	77.66	0.00	100.00								
1.63	31.80	68.20	8.84	91.16	68.18	31.82						
1.44	25.40	74.60	10.87	89.13	55.55							
1.27	17.70	82.30	21.33	78.67	31.82	68.18						
1.10	7.93	92.07	28.29	71.71	41.40	58.60						
0.96	6.73	93.27	39.39	60.61	33,33	66.67	16.67	83.33				
0.84	4.04	95.96	38.92	61.08	44.45	55.55	16.67	83.33	66.67	33.33		
0.68	3.10	96.90	29.42	70.58	42.44	57.56	59. <b>4</b> 5	40.55	23.08	76.92	64.29	35.71
0.57	2.43	97.57	25.14	74.86	37.50	62.50	61.54	38.46	66.67	33,33	52.39	47.61
0.45	3.56	96.44	31.00	69,00	38.80	61.20	62.27	37.73	79.58	20.42	75.52	24.48
0.36	5.58	94.42	47.93	52.07	38.58	61.42	59.76	40.24	47.72	52.28	83.34	16.66
0.28	9.57	90.43	49.53	50.47	32.44	67.56	33.33	66.67	28.51	71.49	28.17	71.83
0.24	16.15	83.85	46.20	53.80	28.12	71.88	18.51	81.49	11.15	88.85	10.67	89.33
0.20	22.80	77.20	52.99	47.01	26.72	73.28	18.45	81.55	5.86	94.14	4.60	95.40
0.15	27.33	72.67	71.90	28.10	32.77	67.23	16.93	83.07	4.91	95.09	2.25	97.75
0.12	95.98	4.02	88.22	11.78	42.00	58.00	23.79	76.21	6.27	93.73	3.54	96.46
0.10	96.91	3.09	92.04	7.96	60.78	39.22	41.44	58.56	11.32	88.68	5.10	94.90
0.08	97.92	2.08	91.95	8.05	74.16	25.84	79.81	20.19	40.12	59.88	11.12	88.88
0.00	98.06	1.94	96.40	3.60	6.32	93.68	98.07	1.93	90.42	9.58	82.98	17.02
Total midd's	13.85	86.15	33.95	66.05	34.43	65.57	28.90	71.10	16.25	83.75	16.28	83.72

of concentrates is so good that it would be accepted by any mill, even the Missouri mills, where such clean concentration is required.

Looking at the middlings (Table XIV.), we see that the quantity is extremely small, and can be made to disappear in a continuous run by feeding them back on to the table without harming either the concentrates or the tailings. They have, however, some very interesting features that are worthy of note. The galena in the 12th run runs high in the coarse and in the fine, and very low in the middle sizes, there being a great heaping-up of quartz in this part. This same point is true in the 16th and 17th runs to a very marked degree. It is again true to a less marked degree in the 14th and 15th runs, and it appears not to be true at all in the 13th run.

Looking at the tailings (Table XV.), we see that run No. 12 stands out pre-eminent, having only 0.29 per cent. of galena in the whole tailings, and the tailings of runs Nos. 13 to 17 are very low in galena, and would probably pass in any concentrating establishment.

We have one feature here which does not and cannot happen in sized runs, Nos. 6 to 11—viz., the tailings get richer in galena down to the finer sizes; but when we look at the tonnage we find that there is scarcely any weight of material down in those sizes, and therefore this loss is not serious and does not bring up the percentage of galena in the final tailings to a serious extent.

Fig. 4 is an ideal sketch of what happens at the discharging-corner of a Wilfley table. Running from coarse on the lower edge to fine on the upper, A, B, C, D, E, F, G, and H represent the different sizes of galena. It appears that they arrange themselves approximately according to this order on the Wilfley table. In like manner, the quartz-grains arrange themselves approximately in order of size, beginning at the lower edge with the largest grade and running smaller and smaller upwards, as indicated by the letters I, J, K, L, M, N, O, and P. The slimes at once take off the galena (H), and the quartz (P). These finest of all grains have not sufficient weight to hold them up to the upper edge, where mathematical logic would place them. They therefore go into the slimes. The next grade, G (galena), and O (quartz), are not fine enough to

Table XV.—Results of Runs Nos. 12 to 17 Computed to Full Size.

NOTE.—The tailings have been sized and weighed and the weights computed in tons and fractions thereof on the 100-ton basis.

						<del></del>
Size.	Run	Run	Run	Run	Run	Run
On.	No. 12.	No. 13.	No. 14.	No. 15.	No. 16.	No. 17.
mm.	Tons.	Tons.	Tons.	Tons.	Tons.	Tons.
2.49	0.042	0.043				
2.06	1.762	1.336	0.056	0.027		
1.63	18.040	18.429	2.083	0.023		0.016
1.44	10.232	21.674	4.434	0.017	0.016	0.011
1.27	8.176	20.207	11.129	0.030	0.016	0.011
1.10	2.828	11.066	9.834	0.071	0.016	0.011
0.96	1.590	7.877	8.167	0.185	0.021	0.022
0.84	1.457	7.835	13.670	0.780	0.026	0.016
0.68	0.281	2.676	13.131	1,843	0.047	0.033
0.57	0.178	2.098	11.080	7.316	0.163	0.044
0.45	0.103	1.122	14.410	21.851	2.381	1.945
0.36	0.021	0.121	4.532	20.371	5.709	5,423
0.28	0.019	0.097	2.604	30.530	34.072	31.480
0.24	0.015	0.038	0.437	5.486	17.393	17.182
0.20	0.017	0.024	0.220	4.473	18.103	19.917
0.15	0.012	0.019	0.087	0.790	10.150	10.175
0.12	0.015	0.014	0.033	0.240	3.129	2.845
0.10	0.002	0.009	0.010	0.084	1.249	0.911
0.08	0.010	0.029	0.010	0.071	0.580	0.544
0.00	0.017	0.029	0.012	0.044	0.169	0.172
Total tons	44.817	94.743	95.939	94.232	93.240	90.758

Analyses of the above products giving percentages of galena (PbS) and quartz (SiO2).

Size,	Run No. 12.		Run No. 13.		Run No. 14.		Run No. 15.		Run No. 16.		Run No. 17.	
On.	Galena.	Quartz.										
mm.	Per Ct.				Per Ct.	Per Ct.						
2.49	0.00	100.00		100.00								·
2.06	0.00	100.00		100.00	0.00	100.00		100.00				
1.63	0.00	100.00	0.08	99.92	0.00	100.00	0.00	100.00				
1.44	0.52	99.48	0.07	99.93	0.09	99.91	0.00	100.00	0.00	100.00	0.00	100.00
1.27	0.20	99.80	0.48	99.52	0.06	99.94	0.00	100.00	0.00	100.00		
1.10	0.38	99.62	0.09	99.91	0.06	99.94	0.00	100.00	0.00	100.00		
0.96	0.67	99.33	0.18	99.82	0.03	99.97	0.00	100.00	0.00	100.00	į	
0.84	0.74	99.26	0.18	99.82	0.03	99.97	0.00	100.00	0.00	100.00	·	i
0.68	0.76	99.24	0.54	99.46	0.02	99.98	0.00	100.00	1.10	98.90		
0.57	1.20	98.80	1.16	98.84	0.02	99.98	0.00	100.00	0.32	99.68	0.00	100.00
0.45	1.03	98.97	6.04	93.96	0.10	99.90	0.17	99.83	0.86	99.14	1.36	98.64
0.36	1.28	98.72	16.00	84.00	0.84	99.16	0.23	99.77	0.45	99.55	0.69	99.31
0.28	7.08	92.92	33.05	66,95	2.08	97.92	0.98	99.02	0.17	99.83	0.34	99.66
0.24	9.22	90.78	27.60	72.40	3.88	96.12	0.27	99.73	0.30	99.70	0.58	99.42
0.20	5.64	94.36	19.00	81.00	5,21	94.79	0.43	99.57	0.35	99.65	0.55	99.45
0.15	5.90	94.10	13.32	86.68	7.73	92.27	3.30	96.70	0.44	99.56	0.54	99.46
0.12	7.50	92.50		84.70	9.59	90.41	8.97	91.03	0.87	99.13	1.01	98.99
0.10	5.40	94.60		59.60	72.79	27.21	17.32		1.83	98.17	2.07	97.93
0.08	28.38	71.62		44.45	21.43		26.55		7.04	92.96	7.38	92.62
0.00	85.93	14.07	87.00	13.00			68.32		42.36	57.64	44.28	55.72
Total tail'gs	0.29	99.71	0.36	99.64	0.20	99.80	0.55	99.45	0.46	99.54	0.66	99.34

go into the slimes nor coarse enough to stand up against the water-current in the position shown in the sketch. These grains are found, therefore, sprinkled through the concentrates, middlings and tailings. See the heaping-up of galena in the small sizes in Tables VIII., IX. and X.

Having laid out our argument in this way, it now remains for us to compare by means of this diagram runs Nos. 1 to 5,

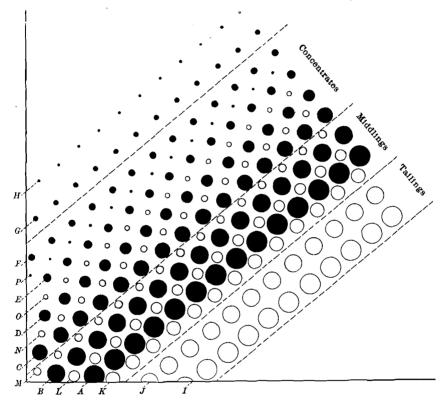


Fig. 4.—Ideal Sketch of the Arrangement of Grains by a Wilfley Table.

6 to 11, and 12 to 17, and to see why it is that runs Nos. 6 to 11 and Nos. 12 to 17 are so much better than runs Nos. 1 to 5. Runs Nos. 1 to 5 take the products just as they are shown in Fig. 4 and give galena, C, D, E, F, in the concentrates contaminated by quartz, (N). See the heaping-up of the quartz a little below the middle size in Table VIII., and the middlings that give quartz, K, L, and M, contaminated by galena, A, B,

C, and G. See the heaping-up of galena among the large grains and among the small grains in Table IX., and the tailings have in them the quartz, I, J, and O, contaminated by galena, G. See the heaping-up of galena in the fine sizes in Table X. Runs Nos. 6 to 11, on the other hand, have put together on the coarse table, quartz, I, and galena, A, which have nothing whatever to do with one another (see Table XII.), and therefore make almost 100 per cent. of galena in the concentrates, and almost 100 per cent. of quartz in the tailings. The little accidental middling-product, simply being the dividing-line between the two products, goes back on the table and disappears. On the second table we treat quartz, J, and galena, B, with the same result. On the third table we treat quartz, K, and galena, C, with the same result. On the fourth table quartz, L, and galena, D; on the fifth table quartz, M, and galena, E; on the sixth table quartz, N, and galena, F. There seems no reason logically why these should not turn out 100 per cent. of galena in the concentrates and 100 per cent. of quartz in the tailings. The probable reason why we did not obtain those figures was that the accidental flat scales and the fine abrasions of galena went where they should not.

Going to the third set of runs, Nos. 12 to 17, we need to bring in an ideal picture of the products of a classifier by means of Fig. 5. Suppose, for example, that we drop into a tall tube of water grains of quartz ranging from our maximum size down to zero, and grains of galena in the same way, and that these grains are of approximately the same shape, then the rate of settling of these grains may be stated in the following terms: the larger grains of a single mineral will settle faster than the smaller grains; and when we compare the two gravities of quartz and galena, the higher gravity will settle faster than the lower gravity for the same size. So definite is this law that if we look for equal-settling particles, we shall find that the grain of quartz which is equal-settling with the grain of galena is about 3 or 4 times the diameter of the grain of galena. See settling-ratios in Table III. We may, therefore, construct the ideal diagram, Fig. 5, and we can draw a set of horizontal lines across it, putting the equal-settling grains together, ranging from the heavier grains of the first spigot in the lower part of the diagram up to the lighter grains of the

finer spigot at the upper part of the diagram. We see then that spigot 1 contains a large amount of galena ranging from the coarsest size down to one-quarter the diameter of the coarsest quartz, and that the quartz is almost all in the coarse sizes. See spigot 1, Table III. This is exactly what we found in our run No. 12. See the heaping-up of galena in the large sizes in Table XIII.

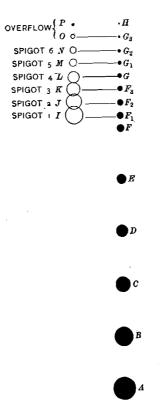


Fig. 5.—Ideal Sketch of Classifier-Product.

Spigot 2 has small galena and large quartz, but both are a little smaller than those in spigot 1. Spigot 3, again, has small galena and larger quartz, but a little smaller than spigot 2, and so on up the scale with spigot 4, spigot 5 and spigot 6. See the heaping-up of galena in smaller sizes, Table XIII., and of quartz in larger sizes in Table XV.

Looking at our diagram, Fig. 5, to see what will happen when these several spigots are put upon the table, we shall find that run No. 12 receives galena, A, B, C, D, E, F, and  $F_1$ , and quartz, I. Logically these have nothing to do with one another, and therefore should make for perfect separation. Spigot 2 fed in run No. 13 would have quartz, J, and galena,  $F_2$ . Spigot 3 would have quartz, K, and galena,  $F_3$ , and so on. Spigots 4, 5, and 6 could work their way up, having quartz always larger, and therefore belonging at a lower place on the table, and galena of smaller diameter belonging at a higher place on the table, making for clean separation of concentrates and tailings, with a middling product that can go directly back on the table and disappear. In proof of this, see points of heaping-up of galena and quartz in Tables XIII. and XV.

In the light of Fig. 4, comparing runs 12 to 17 with runs 6 to 11 we see that the natural lines for quartz and galena are farther apart for the classified products than for the sized products. For example, in run 12 the galena lines A to F average farther from the quartz I than does the galena A of run 6. Again, in run 13 the galena F is farther from quartz J than is the galena B from quartz J in run 7. In like manner we may compare classified runs 14, 15, 16, and 17 with sized runs 8, 9, 10, and 11.

This demonstrates that with perfect classification the work will be better done on the Wilfley table than with sizing, and it also shows that with much middle weight mineral or included grains a good classifier will probably be more efficient than screens.

## Conclusions.

- 1. The natural product as feed for a Wilfley table is completely outclassed and surpassed by sized-product feed and by classifier-product feed.
- 2. While the sized-product feed, as shown in Table VII., appears to have done better work than the classifier-product feed, if we give full weight to the great performance of run No. 12, we can agree that this has fully offset the slight falling-off of runs Nos. 13 to 17, and that the classifier-feed work is fully up to the sized-feed work on the Wilfley table, and with a perfect classifier the work will be better done than with screens.