



**43rd Turbomachinery
30th Pump SYMPOSIA**

GEORGE R. BROWN CONVENTION CENTER
HOUSTON, TX | SEPT. 22 - 25, 2014

CASE STUDY:

Solution for PD Pump Suction Piping System Pulsation/Vibration Problem

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Ray G. Durke – Sr. Research Engineer

Southwest Research Institute



Author's Biography

- **Eugene "Buddy" Broerman** is a Senior Research Engineer with Southwest Research Institute (SwRI). He has nearly 13 years of experience with pulsation/vibration related problems. He holds a bachelor's degree in mechanical engineering from Texas A&M University – Kingsville. Contact him at: EBroerman@swri.org
- **Ray Durke** is a Senior Research Engineer with Southwest Research Institute (SwRI). He has 35 years experience in plant dynamics, primarily in diagnosing and correcting machinery vibration and pulsation-related problems. He holds a BSME from Texas A&M University and an MBA from UTSA. Contact him at: rdurke@swri.org

Agenda

- Introduce System & Problem
- Steps taken to Solve Problem
- Summary & Lessons Learned

Pump Description Details

Pumps Details

2 pumps (plunger)
Separate piping systems

3 plungers per pump

3.375" bore (8.57 cm)

5" stroke (12.7 cm)

166 rpm

Pump Operating Conditions

Suction Pressure:
30-40 psig (2.1-2.8 barg)

Discharge Pressure:
1000-1250 psig (69-86 barg)

Temperature:
210-230°F (99-110°C)

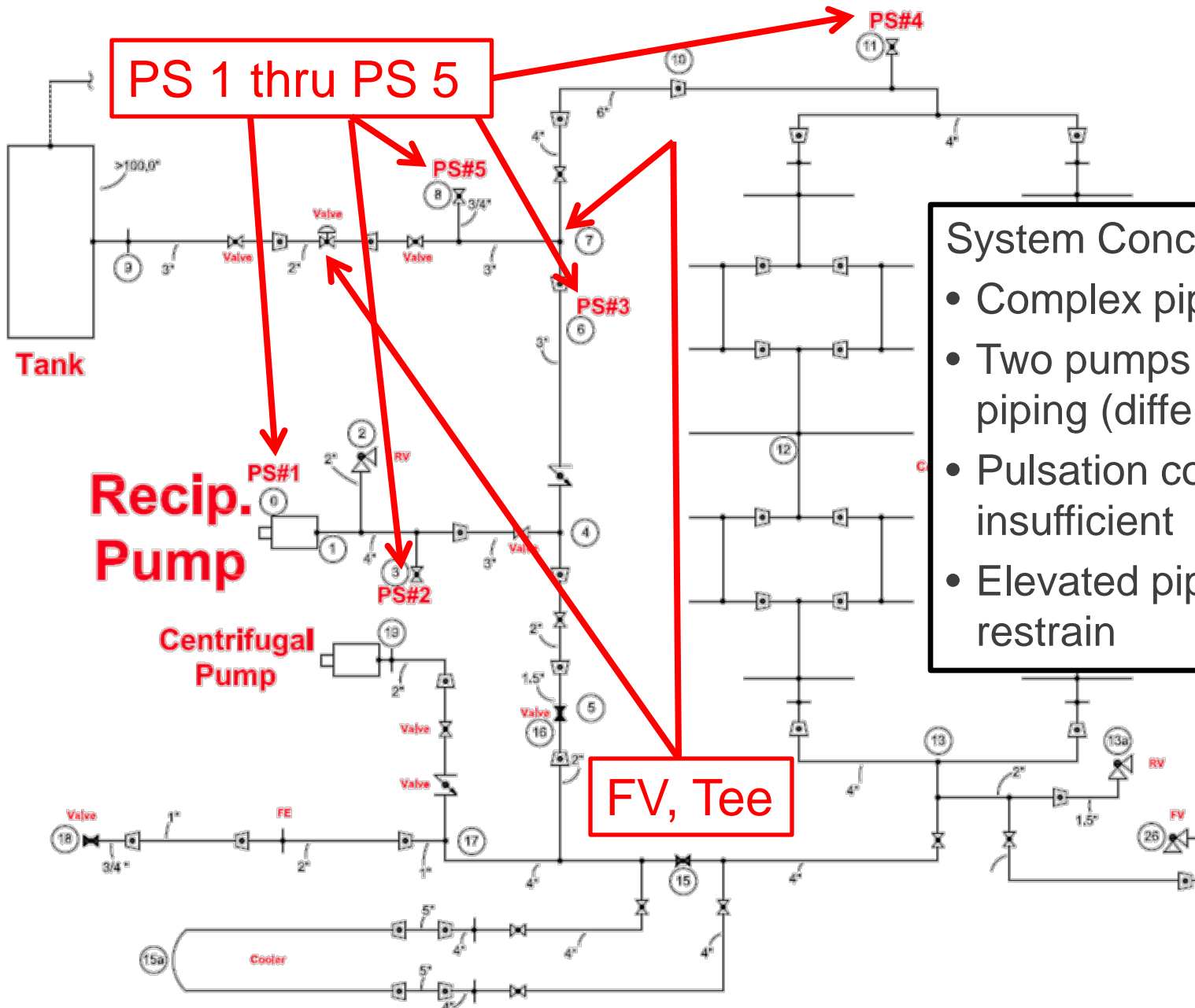
Problems

- High suction piping vibration causing:
 - Pipe insulation deterioration
 - Pipe restraint damage
 - Shortened pump valve life
 - High noise
- Gas-liquid pulsation dampeners installed years prior to field investigation – removed due to high maintenance and frequent bladder failures
- Issues above raised safety & reliability concerns

Steps Taken to Solve Problem

- Field investigation for problem characterization and diagnostics – vibration & pulsation data measured
- Pulsation analysis conducted to develop potential solutions
- Maintenance-free, all-liquid acoustic filter bottle recommended

Piping Layout



System Concerns:

- Complex piping system
- Two pumps with similar piping (different services)
- Pulsation control insufficient
- Elevated pipe difficult to restrain

Summary of Field Measured Pulsation & Estimated Forces

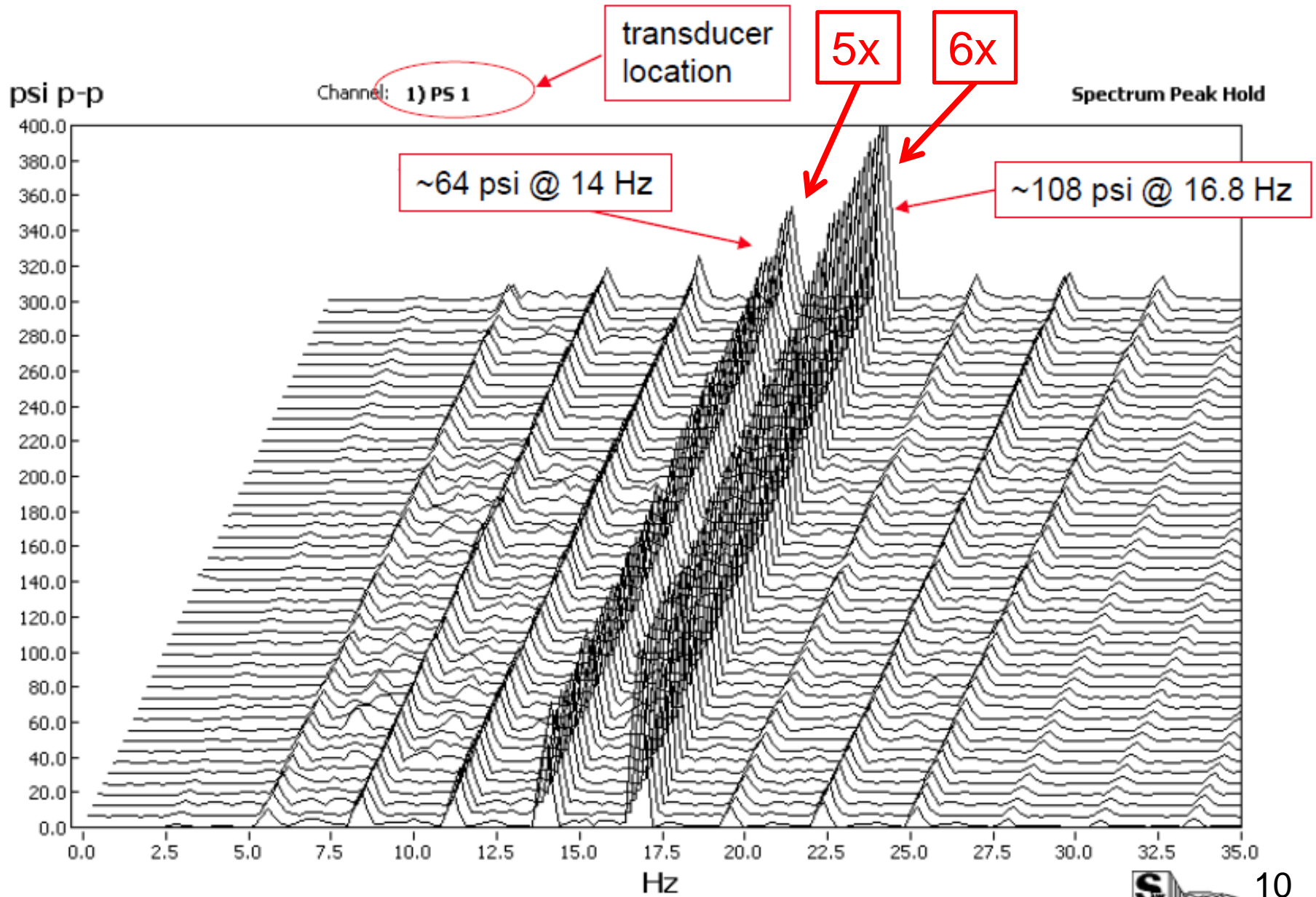
Test Point	Overall Amplitudes		Pulsation (psi p-p) at Discrete Frequencies			
	Pulsation psi pk-pk	Shaking Force lb _f p-p	3x	5x	6x	~10x
PS 1	110	1749	22	64	108	--
PS 2	143	1820	19	60	96	--
PS 3	----- No signal -----					
PS 4	45	573	15	--	95	--
PS 5	80	591	11	--	17	24 / 25

Indicates potential of failed valves

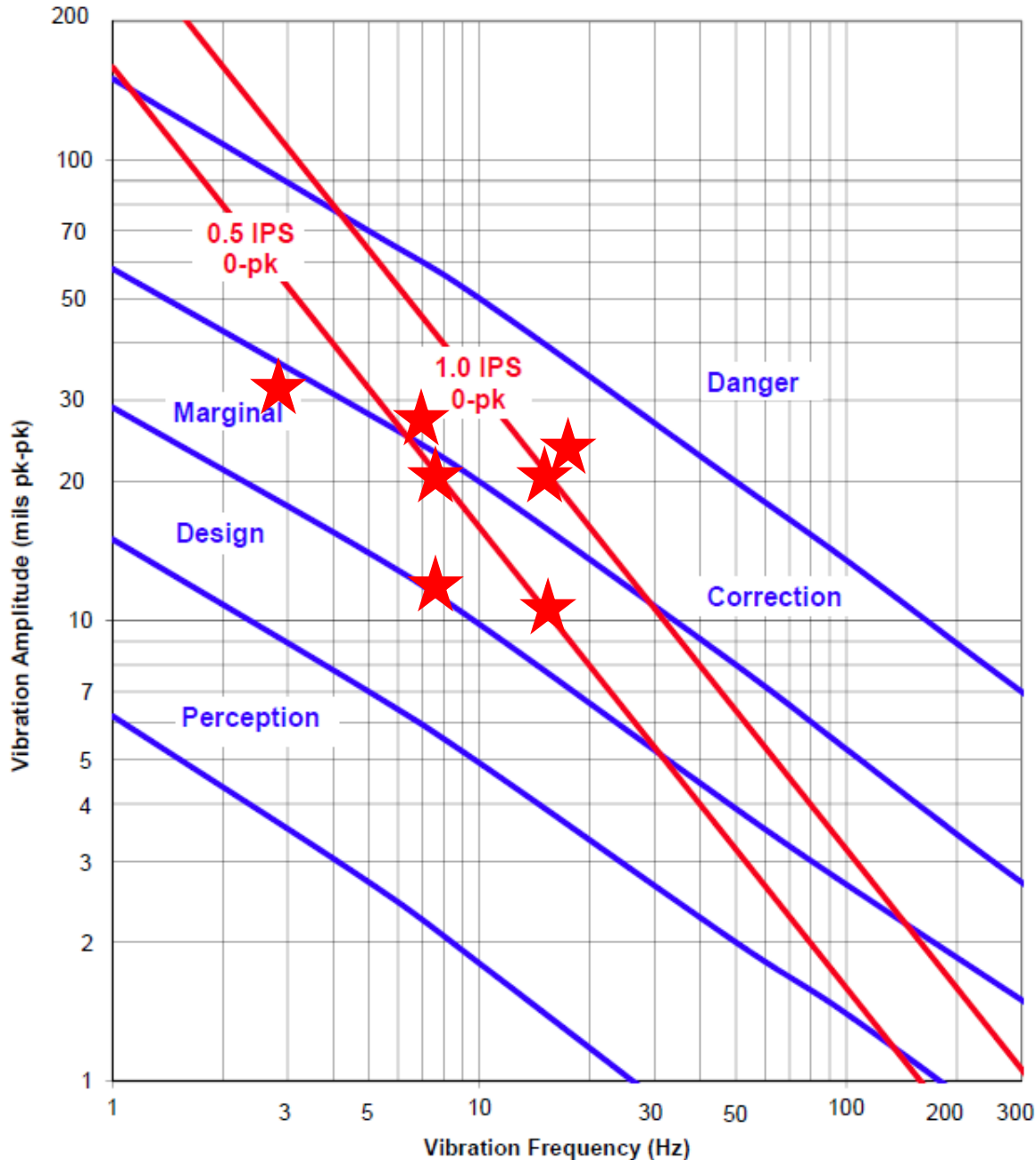
Summary of Field Measured Vibration

Test Point	Overall Amplitude	Vibration (mils p-p) at Discrete Frequencies				
	Vibration mils p-p	1x	3x	5x	6x	7 Hz
FV E-W	45	11	4	10	3	--
Tee E-W	65	--	20	20	13	26
Tee N-S	65	31	11	9	22	--

Field Pulsation Data at Pump



Southwest Research Institute Screening Piping Vibration Severity Chart



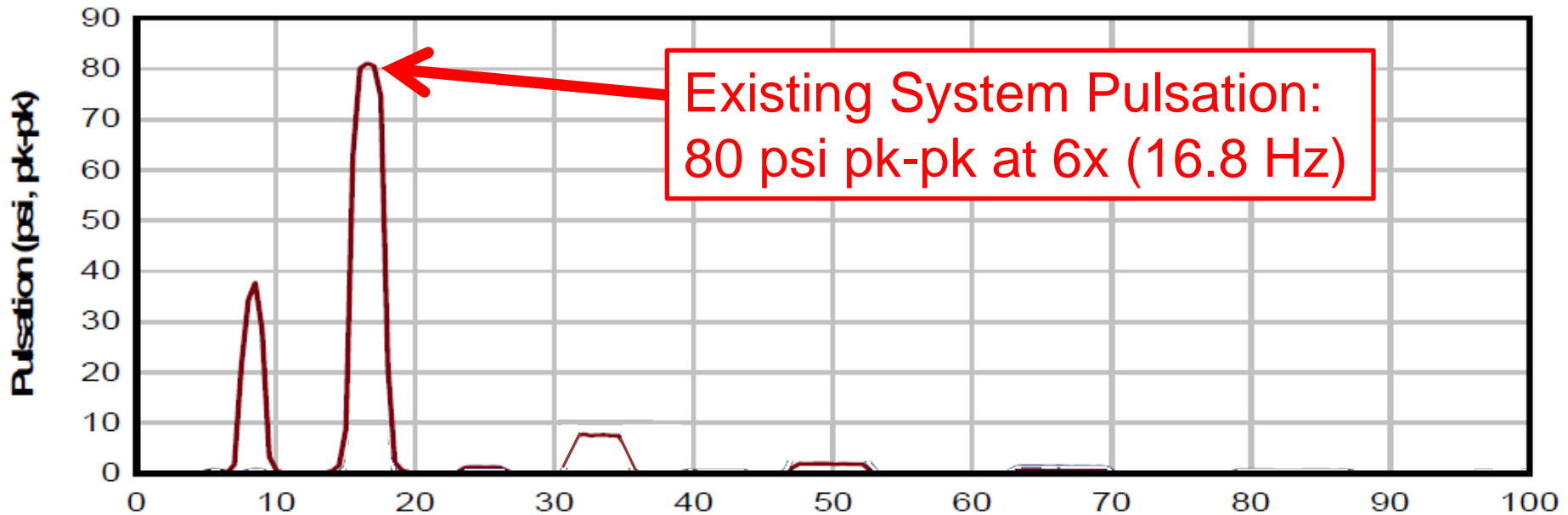
Field Vibrations on SwRI Vibration Guideline Chart

Field measured vibrations in “Marginal” and “Correction” regions

Pulsation Model Results

Highest pulsation amplitudes predicted at 6x running speed:

- at pump manifold: 80 psi pk-pk
- in upstream piping: ~ 11 to 80 psi pk-pk

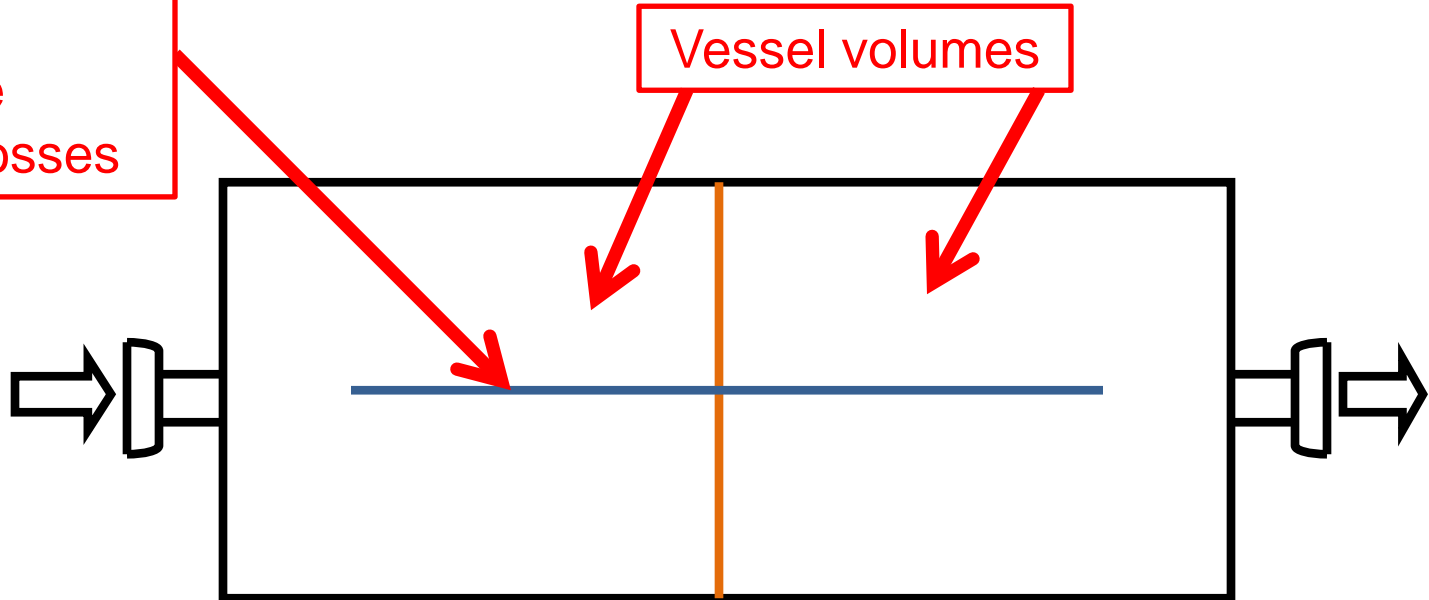


All-liquid Acoustic Filter

Note: Original gas-liquid pulsation dampeners removed due to high maintenance and frequent bladder failures

Choke tube
sized for
acceptable
pressure losses

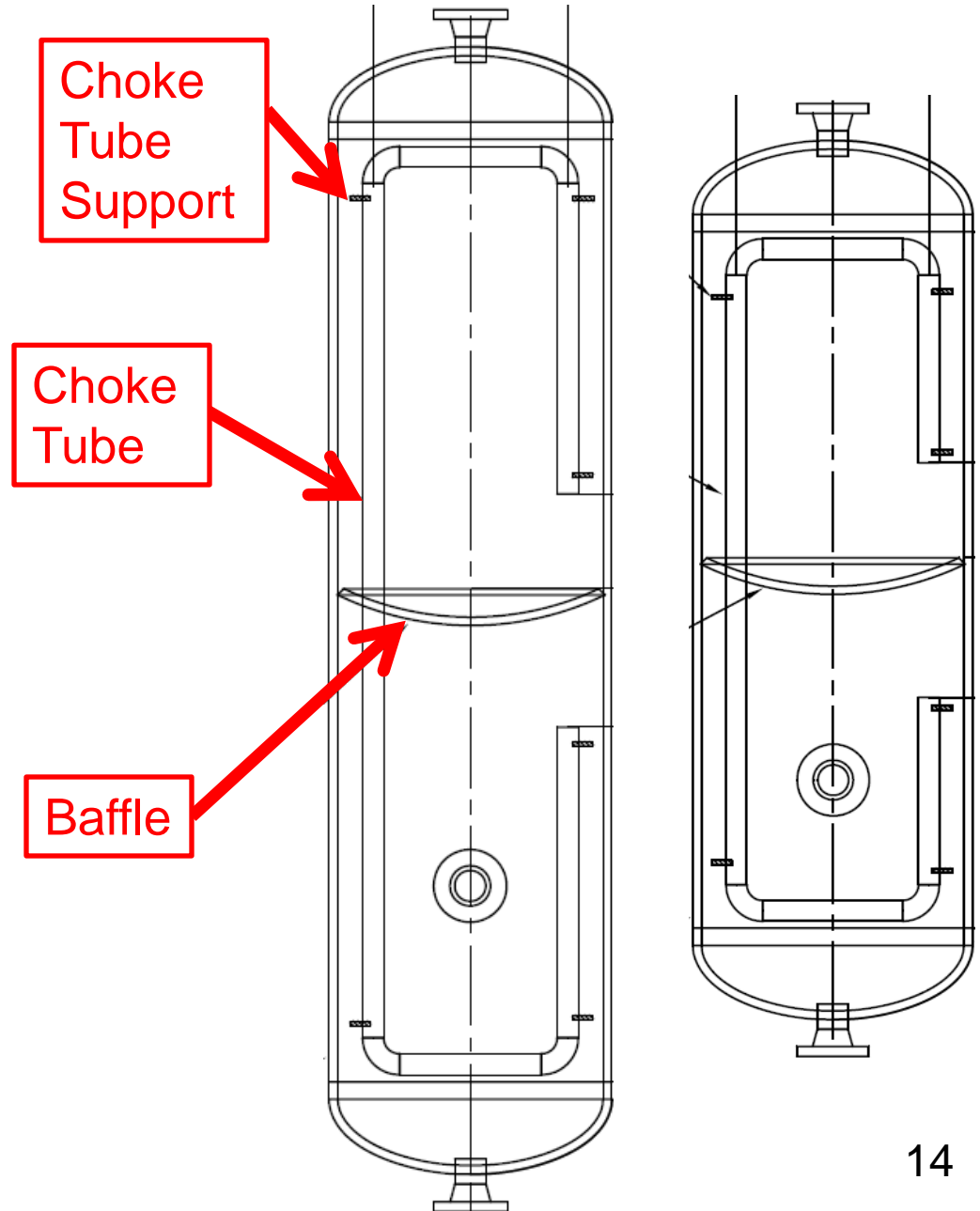
Vessel volumes



Filter sized to attenuate pulsations at plunger frequency (3x running speed) and at higher harmonics

Acoustic Filter Details

- Recommended bottle
 - ~9-feet seam-to-seam
 - ~30" diameter
- Choke Tube
 - Nearly 20-feet long
- Different size filter for each pump due to different services



Equation – Acoustic Filter

$$f_H = \frac{c}{2\pi} \left(\frac{\mu}{V_1} + \frac{\mu}{V_2} \right)^{\frac{1}{2}} \quad \mu = \frac{A}{L}$$

f_H = Helmholtz frequency (Hz)

A = Cross-sectional area of choke (ft²)

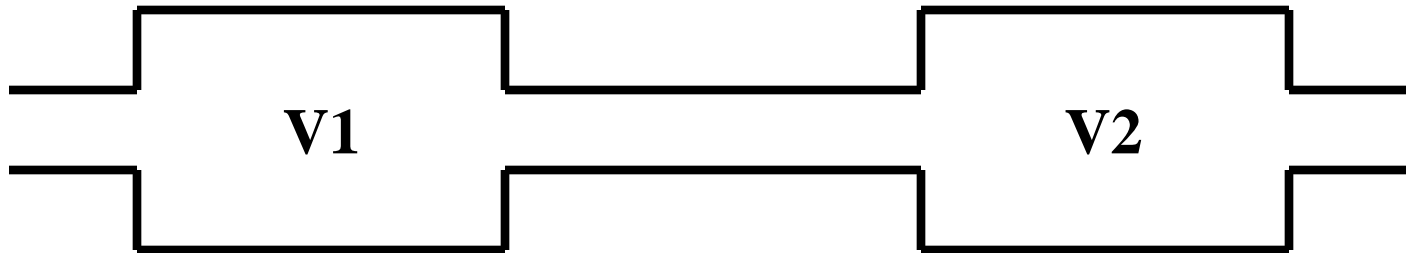
L = Acoustic length of choke (ft)

c = Velocity of sound (ft/sec)

V_1 = Volume of cylinder bottle or chamber (ft³)

V_2 = Volume of filter bottle or chamber (ft³)

- Green = Geometry
- Red = Operating conditions property

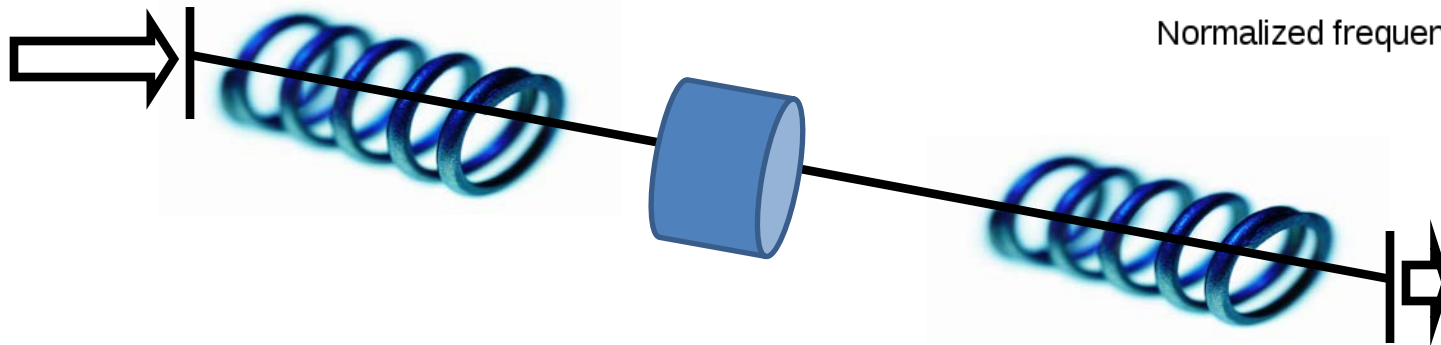
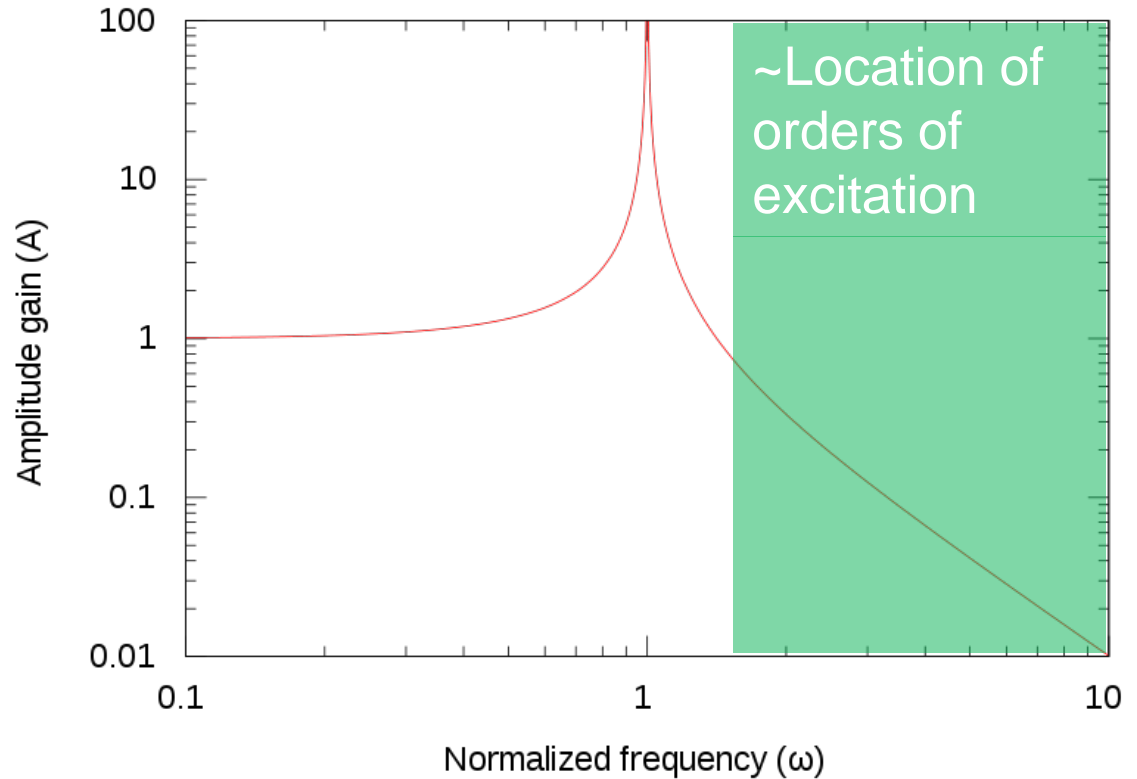


General Concept of an Acoustic Filter

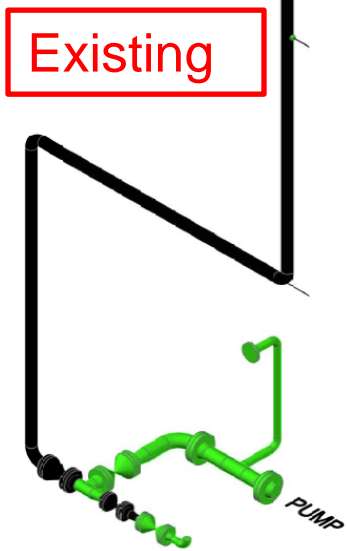
Analogous to low-pass electrical filter or **mechanical spring-mass system**

- Volume = Spring
- Choke tube = Mass

Frequency response of ideal harmonic oscillator

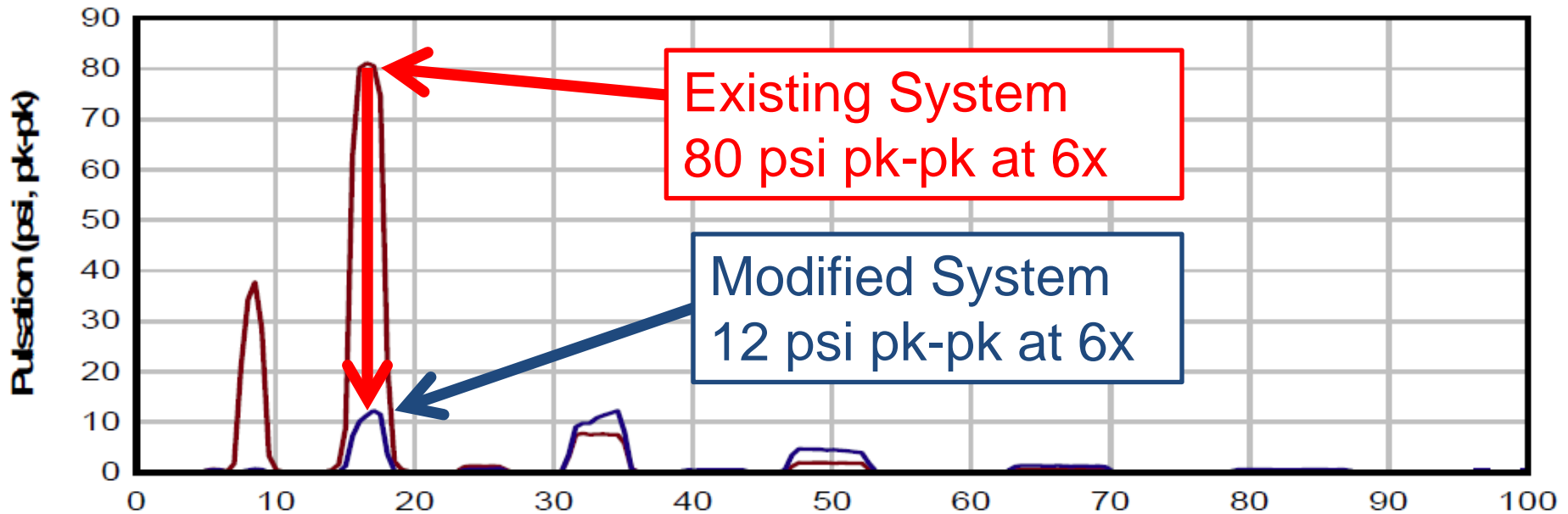
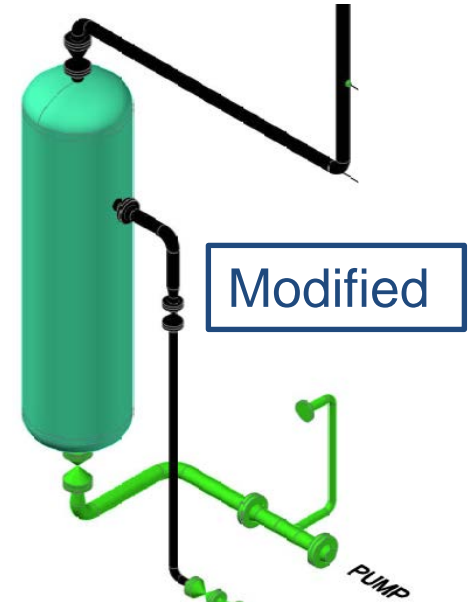


Pulsation Model Results – Modified System



Maximum amplitude pulsations reduced with filter:

- Pump manifold: **12** psi pk-pk
- in upstream piping: **0.1-12** psi pk-pk



Vibrations with Filter Installed

Test Point	<u>Before</u> 3x (mils pk-pk)	<u>After</u> 3x (mils pk-pk)
FV	79	0.73
Pump Suction	34	0.37
Pump Discharge	33	1.25

- Data measured by operating company
- Highest vibration with filter = 1.8 mils pk-pk at 9x on disch. pipe

The following is a quote from the client:

“operators saying they have to walk up and touch the motor to make sure it’s running... whereas they could hear the pump from the road, before the change.”

Summary and Lessons Learned

- Pump System Problem
 - High amplitude piping vibrations
 - Insulation and restraint damage
 - Gas-liquid dampener bladder failures
- Steps taken to Solve Problem
 - Field investigation for problem evaluation – vibration & pulsation measurements
 - Pulsation analysis
- Summary & Lessons Learned
 - All-liquid acoustic filter can significantly reduce system pulsation and vibration amplitudes

Questions/Comments?

Please ask. If you have a question, someone else in the room probably has a question also.

